

Transfer-Matrix Method

$$k_x^2 + k_z^2 = \omega^2 \mu_0 \epsilon + i \mu_0 \sigma \omega = \left(\frac{\omega}{c}\right)^2 n^2, \quad \text{where } n \text{ is the refractive index, giving}$$

$$k'_x = \sqrt{\epsilon_r + i \frac{\sigma}{\epsilon_0 \omega} - k_z^2} \quad \text{where } k = \frac{\omega}{c} k' , \quad k'_z = n_0 \sin(\theta), \quad (n_0 \text{ is } n \text{ for the first layer})$$

TE-polarisation (E parallel to interface, i.e. $E_x = E_z = 0$; $H_y = 0$; only consider tangential H_z term)

$$E_y = (A e^{-i k_x x} + B e^{i k_x x}) e^{-i \omega t} e^{i k_z z}$$

$$\vec{H} = \frac{-i}{\mu_0 \omega} \vec{\nabla} \times \vec{E} \quad \text{i.e.} \quad \begin{pmatrix} E_y(x) \\ H_z(x) \end{pmatrix} = \begin{pmatrix} e^{-i k_x x} & e^{i k_x x} \\ -k'_x e^{-i k_x x} & \frac{k_x}{\omega \mu_0} e^{i k_x x} \end{pmatrix} \begin{pmatrix} A \\ B \end{pmatrix}$$

$$H_z = \frac{k_x}{\mu_0 \omega} (-A e^{-i k_x x} + B e^{i k_x x})$$

Multiply H terms by $c \mu_0$ to get $\begin{pmatrix} E_y(x) \\ c B_z(x) \end{pmatrix} = \begin{pmatrix} e^{-i k_x x} & e^{i k_x x} \\ -k'_x e^{-i k_x x} & k'_x e^{i k_x x} \end{pmatrix} \begin{pmatrix} A \\ B \end{pmatrix} = m \vec{b}$, which gives

$$\vec{b}_{j+1} = \begin{pmatrix} e^{-i k_{j+1} x} & e^{i k_{j+1} x} \\ -k'_{j+1} e^{-i k_{j+1} x} & k'_{j+1} e^{i k_{j+1} x} \end{pmatrix}^{-1} \begin{pmatrix} e^{-i k_j x} & e^{i k_j x} \\ -k'_{j+1} e^{-i k_j x} & k'_{j+1} e^{i k_j x} \end{pmatrix} \vec{b}_j = m_{j+1}^{-1} m_j \vec{b}_j$$

$\vec{b}_{j+1} = M_j \vec{b}_j$ i.e. $\vec{b}_R = M_j M_{j-1} \dots M_1 \vec{b}_L$ for j interfaces

$$\begin{pmatrix} 0 \\ t \end{pmatrix} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \begin{pmatrix} r \\ 1 \end{pmatrix} \quad \text{giving} \quad r = \frac{-M_{12}}{M_{11}} \quad \text{and} \quad R = |r|^2$$

$$t = M_{22} - \frac{M_{21} M_{12}}{M_{11}}$$

TM-polarisation (H parallel to interface, i.e. $H_x = H_z = 0$; $E_y = 0$; only consider tangential E_z term)

$$H_y = (A e^{-i k_x x} + B e^{i k_x x}) e^{i(k_z z - \omega t)}$$

$$\vec{\nabla} \times \vec{H} = \vec{J} + \epsilon \frac{\partial \vec{E}}{\partial t} = (\sigma - i \omega \epsilon) \vec{E} \quad \text{i.e.} \quad \begin{pmatrix} H_y(x) \\ E_z(x) \end{pmatrix} = \begin{pmatrix} e^{-i k_x x} & e^{i k_x x} \\ -i k_x e^{-i k_x x} & \frac{i k_x}{(\sigma - i \omega \epsilon)} e^{i k_x x} \end{pmatrix} \begin{pmatrix} A \\ B \end{pmatrix}$$

$$E_z = \frac{i e^{i k_z z}}{(\sigma - i \omega \epsilon)} (-k_x A e^{-i k_x x} + k_x B e^{i k_x x})$$

from the top of the page $\sigma - i \omega \epsilon = -i \epsilon_0 \omega n^2$ and $k = \frac{\omega}{c} k'$, and so:

$$\begin{pmatrix} H_y(x) \\ c \epsilon_0 E_z(x) \end{pmatrix} = \begin{pmatrix} e^{-i k_x x} & e^{i k_x x} \\ k'_x e^{-i k_x x} & -k'_x e^{i k_x x} \end{pmatrix} \begin{pmatrix} A \\ B \end{pmatrix}$$

$$\text{This means that } \vec{b}_{j+1} = \begin{pmatrix} e^{-i k_{j+1} x} & e^{i k_{j+1} x} \\ k'_{j+1} e^{-i k_{j+1} x} & -k'_{j+1} e^{i k_{j+1} x} \end{pmatrix}^{-1} \begin{pmatrix} e^{-i k_j x} & e^{i k_j x} \\ k'_{j+1} e^{-i k_j x} & -k'_{j+1} e^{i k_j x} \end{pmatrix} \vec{b}_j = M_j \vec{b}_j$$

and so on identically as in the TE-case.

P.T.O.

Manual Calculations

Case 1 – R,T for ...n_L=1|n_R=1.5... for incident rays, TE and TM at 1550nm

TE:

$$M = \begin{pmatrix} 1 & 1 \\ -1.5 & 1.5 \end{pmatrix}^{-1} \begin{pmatrix} 1 & 1 \\ -1 & 1 \end{pmatrix} = \begin{pmatrix} \frac{5}{6} & \frac{1}{6} \\ \frac{1}{6} & \frac{5}{6} \end{pmatrix} \quad (\text{k}' = n \text{ for incident rays, since } k_z = 0)$$

$$R = \left| \frac{1/6}{5/6} \right|^2 = 0.04 \quad \text{which both match my program's output}$$

$$T = \left| \frac{5}{6} - \frac{(1/6)(1/6)}{5/6} \right|^2 = 0.64$$

TM:

$$M = \begin{pmatrix} 1 & 1 \\ \frac{1.5}{1.5^2} & \frac{-1.5}{1.5^2} \end{pmatrix}^{-1} \begin{pmatrix} 1 & 1 \\ \frac{1}{1^2} & \frac{-1}{1^2} \end{pmatrix} = \begin{pmatrix} 1 & 1 \\ \frac{1}{1.5} & \frac{-1}{1.5} \end{pmatrix}^{-1} \begin{pmatrix} 1 & 1 \\ 1 & -1 \end{pmatrix} = \begin{pmatrix} \frac{5}{4} & \frac{-1}{4} \\ \frac{-1}{4} & \frac{5}{4} \end{pmatrix}, \quad R = \left| \frac{-(-1/4)}{5/4} \right|^2 = 0.04$$

$$T = \left| \frac{5}{4} - \frac{(-1/4)(-1/4)}{5/4} \right|^2 = 1.44$$

which both match my program's output

(Note that R_{TM} = R_{TE}, T_{TM} ≠ T_{TE}, and that T_{TM} > 1)

Case 2 – R,T for ...n_L|n_R... for incident rays, TE and TM at 1550nm, varying n_R/n_L

Note: using different ratios for TE- and TM- ; ratios which demonstrate T>1 for each polarisation

TE, n_L=2, n_R=1

$$M = \begin{pmatrix} 1 & 1 \\ -1 & 1 \end{pmatrix}^{-1} \begin{pmatrix} 1 & 1 \\ -2 & 2 \end{pmatrix} = \begin{pmatrix} \frac{3}{2} & \frac{-1}{2} \\ \frac{-1}{2} & \frac{3}{2} \end{pmatrix}, \quad R = \left| \frac{-(-1/2)}{(3/2)} \right|^2 = \frac{1}{9}$$

$$T = \left| \frac{3}{2} - \frac{(-1/2)(-1/2)}{3/2} \right|^2 = 1\frac{7}{9}$$

both of which match my program's output

TM, n_L=1, n_R = 2

$$M = \begin{pmatrix} 1 & 1 \\ \frac{2}{2^2} & \frac{-2}{2^2} \end{pmatrix}^{-1} \begin{pmatrix} 1 & 1 \\ \frac{1}{1^2} & \frac{-1}{1^2} \end{pmatrix} = \begin{pmatrix} 1 & 1 \\ \frac{1}{2} & \frac{-1}{2} \end{pmatrix}^{-1} \begin{pmatrix} 1 & 1 \\ 1 & -1 \end{pmatrix} = \begin{pmatrix} \frac{3}{2} & \frac{-1}{2} \\ \frac{-1}{2} & \frac{3}{2} \end{pmatrix}, \quad R = \left| \frac{-(-1/2)}{(3/2)} \right|^2 = \frac{1}{9}$$

$$T = \left| \frac{3}{2} - \frac{(-1/2)(-1/2)}{3/2} \right|^2 = 1\frac{7}{9}$$

which both match my program's output

(Note that T > 1 for TE- and TM- polarisations)