

## LIST OF EQUATIONS

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Note: Not all of these equations are required for the examination.

$$\sigma_{x'} = \sigma_x \cos^2 a + \sigma_y \sin^2 a + \tau_{xy} \sin 2a$$

$$\sigma_{y'} = \sigma_x \sin^2 a + \sigma_y \cos^2 a - \tau_{xy} \sin 2a$$

$$\tau_{x'y'} = \left( \frac{\sigma_y - \sigma_x}{2} \right) \sin 2a + \tau_{xy} \cos 2a$$

$$\varepsilon_{x'} = \varepsilon_x \cos^2 \alpha + \varepsilon_y \sin^2 \alpha + \frac{\gamma_{xy}}{2} \sin 2\alpha$$

$$\frac{\gamma_{x'y'}}{2} = \frac{\varepsilon_y - \varepsilon_x}{2} \sin 2\theta + \frac{\gamma_{xy}}{2} \cos 2\theta$$

$$\varepsilon_{1,2} = \varepsilon_{\max, \min} = \frac{\varepsilon_x + \varepsilon_y}{2} \pm \sqrt{\left( \frac{\varepsilon_x - \varepsilon_y}{2} \right)^2 + \left( \frac{\gamma_{xy}}{2} \right)^2} \quad \tan 2\alpha = \frac{2 \left( \frac{\gamma_{xy}}{2} \right)}{\varepsilon_x - \varepsilon_y}$$

$$\frac{\gamma_{\max}}{2} = \frac{\varepsilon_1 - \varepsilon_2}{2}$$

$$\sigma_{1,2} = \sigma_{\max, \min} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left( \frac{\sigma_x - \sigma_y}{2} \right)^2 + \tau_{xy}^2} \quad \tan 2\alpha = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

$$\tau_{\max} = \frac{\sigma_1 - \sigma_2}{2}$$

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**General Constitutive  
Equations;**

$$\varepsilon_x = \frac{1}{E} [\sigma_x - \nu (\sigma_y + \sigma_z)] \quad \tau_{xy} = G \gamma_{xy}$$

$$\varepsilon_y = \frac{1}{E} [\sigma_y - \nu (\sigma_x + \sigma_z)] \quad \tau_{xz} = G \gamma_{xz}$$

$$\varepsilon_z = \frac{1}{E} [\sigma_z - \nu (\sigma_x + \sigma_y)] \quad \tau_{yz} = G \gamma_{yz}$$

$$\sigma_x = \lambda \varepsilon_v + 2G \varepsilon_x$$

$$\sigma_y = \lambda \varepsilon_v + 2G \varepsilon_y$$

$$\sigma_z = \lambda \varepsilon_v + 2G \varepsilon_z$$

$$\lambda = \frac{\nu E}{(1+\nu)(1-2\nu)} \quad G = \frac{E}{2(1+\nu)}$$

$$\varepsilon_v = \varepsilon_x + \varepsilon_y + \varepsilon_z$$

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Constitutive Equations  
(Plane Stress conditions):

$$\sigma_x = \frac{E}{(1-\nu^2)} [\epsilon_x + \nu \epsilon_y]$$

$$\tau_{xy} = G \gamma_{xy}$$

$$G = \frac{E}{2(1+\nu)}$$

$$\sigma_y = \frac{E}{(1-\nu^2)} [\epsilon_y + \nu \epsilon_x]$$

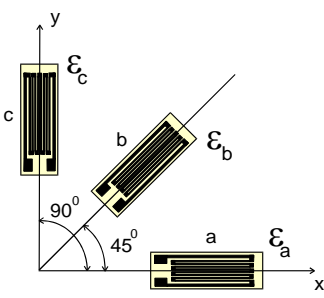
Spherical Pressure Vessels  $\sigma_1 = \sigma_2 = \frac{pr}{2t}$

Cylindrical Pressure Vessels  $\sigma_1 = \frac{pr}{t}; \sigma_2 = \frac{pr}{2t}$

Von Mises Failure Criteria (plane stress)  $\sigma_1^2 + \sigma_2^2 - \sigma_1 \sigma_2 < \sigma_{Yield}^2$

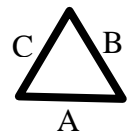
Tresca Failure Criteria (plane stress)  $\tau_{max} \leq \frac{\sigma_{yield}}{2}$

Maximum Principle stress Failure criteria  $\sigma_{max} < \sigma_{ult}$



$$\gamma_{xy} = 2\epsilon_b - \epsilon_c - \epsilon_a, \quad \epsilon_x = \epsilon_a, \quad \epsilon_y = \epsilon_c$$

For 60° rosette  $\gamma_{xy} = \frac{2}{\sqrt{3}}(\epsilon_C - \epsilon_B)$  and  $\epsilon_y = \frac{2}{3}\left(\epsilon_B + \epsilon_C - \frac{\epsilon_A}{2}\right)$  and  $\epsilon_x = \epsilon_a$



$$\tau = \frac{VA\bar{y}}{Ib} \quad \sigma = \frac{My}{I} \quad I_{\text{rectangle}} = \frac{bh^3}{12} \quad I_{xx} = I_{11} + A\bar{y}^2 \quad EI \frac{d^2y}{dx^2} = M$$

|                       |  |                   |
|-----------------------|--|-------------------|
| First Yield Moment:   | $M_y = Zf_y$                           | $Z = \frac{I}{y}$ |
| Fully Plastic Moment: | $M_p = Sf_y$                           |                   |
| Shape Factor:         | $\eta = \frac{M_p}{M_y} = \frac{S}{Z}$ |                   |

**Moment area Theorem 1:**  $\theta_B - \theta_A = \text{Area} \frac{M}{EI}$

**Moment area Theorem 2:** If a vertical line is drawn at any location D, and tangents are produced from A and B to intersect this line, the distance between the points of intersection is equal to the first moment of area of that portion of the M/EI diagram between A and B, taken with respect to that line.

