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## Assumptions and Important Workflow Notes

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```
% We will begin by Separating System Into Control Volumes
% 1) Compression chamber 2) Expansion chamber 3) Piston FBD, and
% 4) annular area
%
% Each system will be iteratively processed using form of Eulers
% I.E one iteration passes, how much flow from one sealed sys to the other
% After taking each iteration into effect, find the total flow,
% compare to removed volume
%
```

## Define and Clear Variables

---

```
% Clear Variables
clc, clear, clear all,;
```

```

Di = 11.25;      % In

%while loop used to analyze varying inside diameters
while Di<12.249;

```

```

Di = Di+.125;    % In
Do = 12.25;      % In
L1 = 13.35;      % In
L2 = 10.95;      % In
syms x;          % In

% Air Properties
gamma = 1.6;      % specific gravity
K1 = 1.4;          % spc heat
R = 40.87;         % Gas constant inlb/molR
MolM = .063845;   % molecular mass lb/mol
u = .00000000263; % lbf*sec/in2 dynamic viscosity assumed constant

```

## Compressed Area CV

---

Derive from first law  $\Delta U = Q - W$  assume control volume with no exit, sealed adiabatic rapid compression

```

Apiston = pi*(Di/2)^2;           % In2
V0 = (pi*(Do/2)^2)*((L1-L2)/2); % Initial chamber volume, In3
V1c = V0;                      % Vol of comp chamber before compression
V2c = V0-Apiston*x;            % Vol of comp chamber after compression
P1c = 14.7; % Pressure of initial compression lb/in2

% work of piston is equal to integral pdv (neg for comp)
% W = Fd=int(Pdv) :: W=.5*k*(x^2)=int(Pdv) (note W=fdx)
% Pvk =C, integrating yeilds W=Fd=(P2V2-P1V1)/(1-k)

PC = (((-.5*Ks*x*x)*(1-K1))+P1c*V1c)/(V2c); %lb/in

```

## Expanded Area CV

---

Derive from first law  $\Delta U = Q - W$  assume control volume with no exit, sealed adiabatic rapid expansion

```

Apiston = pi*(Di/2)^2;
V0 = (pi*(Do/2)^2)*((L1-L2)/2);
V1x = V0;
V2x = V0+Apiston*x;
P1x = 14.7;                                % same scenario as compressed

% work of piston is equal to integral pdv (pos for expansion)
% W = Fd=int(Pdv) :: W=.5*k*(x^2)=int(Pdv) (note W=fdx
% Pv^k =C, integrating yeilds W=Fd=(P2V2-P1V1)/(1-k)

Px = (((.5*Ks*x*x)*(1-K1))+P1x*V1x)/(V2x);    % lb/in

```

## Annular Area CV

We will use Darcy Weisbach equations to compute pressure loss and flow rate in equivulant hydrodynamic pipe

```

% calculate Dh hydraulic area
Dh = Do-Di;

% calculate Temperature at entrance T2/T1 = V1/V2^n-1 (ideal, adiabatic)
Tx = 500*((V1x/V2x)^.4);      % 500 is reasonable initial cond in deg R
Tc = 500*((V1c/V2c)^.4);
Tavg = (Tx+Tc)/2;

%calculate ave density in annular pv=mrt=nrt rho=m/v
Achamber = pi*(Do/2)^2;
Aannular = Achamber-Apiston;          % annular area is disc between case and inside piston
Vannular = (Aannular)*L2;            % in3
n=((Px+Pc)/2)*Vannular/(40.87*Tavg); % mol
m=n*MolM;                          % lb
rho = m/Vannular;                  % lb/in3

%Assume turbulent, roughness e = .025mm.
fd = .0275;
DeltaP = Pc-Px;
Vel2 = sqrt(DeltaP*2*Dh/(fd*L2*rho));    % Darcy Weisbach based on delta Pressure
Vdot = Vel2*Aannular;                    % in3/sec the volume flow rate

```

## Compare displaced air volume to escaped volume

---

This will find the pressure n plate due to compressed air

```

StrokeTime = x/24;                                % sec, 24 is vel of stroke

Vescape = Vdot*StrokeTime;                         % all velocities in in/sec
Vremoved = Apiston*x;
Vcompressed = Vremoved - Vescape;
Vchamber=Achamber*((L1-L2)/2))-Vremoved;

n2=.01639706*(Vcompressed+Vchamber)/22.4;        % number moles
Pressure = n2*40.87*Tavg/((Vchamber));           % psi
Force = Pressure / Apiston;                        % lb

```

## Compute time iteration for each changing volume flow

---

```

z=0;

while z<.6

    % we are assaigning the variable sym x some distance value z
    % the will influence each following calculation

    z=z+.02;                                     % distances of stroke
    nV2c = subs(V2c,x,z);
    nPc=subs(Pc,x,z);
    nV2x =subs(V2x,x,z);
    nPx =subs(Px,x,z);
    nTx =subs(Tx,x,z);
    nTc=subs(Tc,x,z);
    nTavg=subs(Tavg,x,z);

    nn=subs(n,x,z);
    nm=subs(m,x,z);
    nrho=subs(rho,x,z);

    nDeltaP=subs(DeltaP,x,z);
    nVel2=subs(Vel2,x,z);
    nVdot=subs(Vdot,x,z);

```

```
nStrokeTime=subs(StrokeTime,x,z);
nVremoved=subs(Vremoved,x,z);
nVcompressed=subs(Vcompressed,x,z);
nVchamber=subs(Vchamber,x,z);
nn2=subs(n2,x,z);
nPressure=subs(Pressure,x,z);
nForce=subs(Force,x,z);

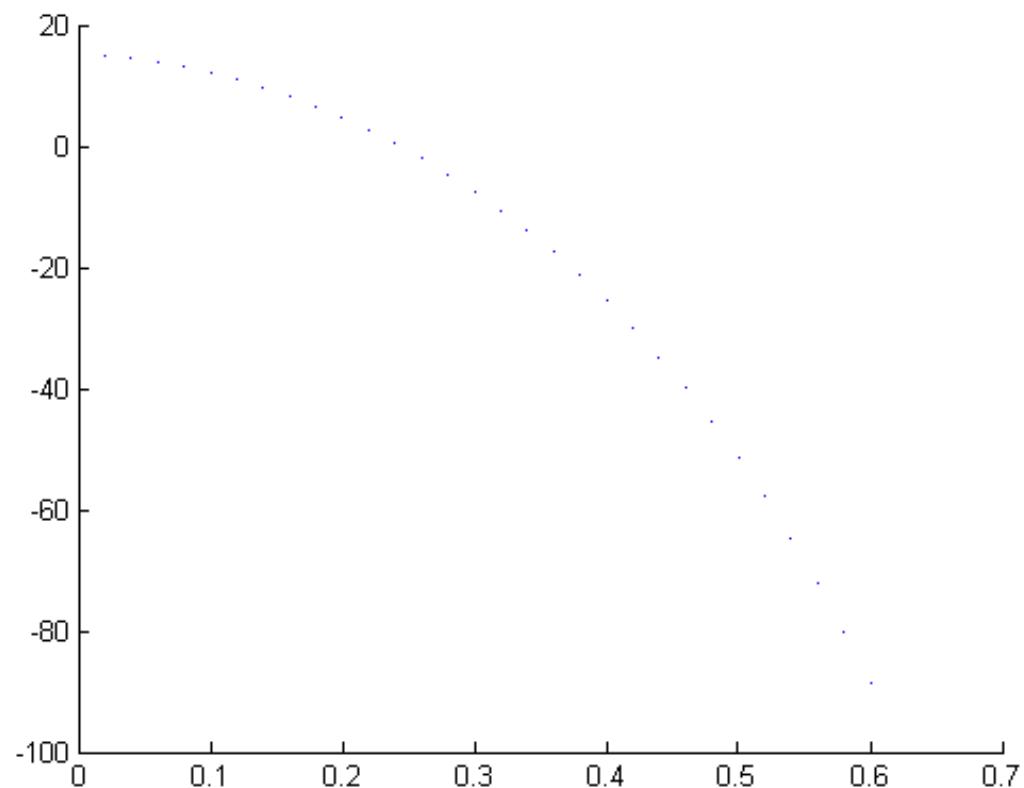
% set the intitial pressure to the new pressure
% this changes much of the next calculation, and
% ultimately the amount of gas not compressed

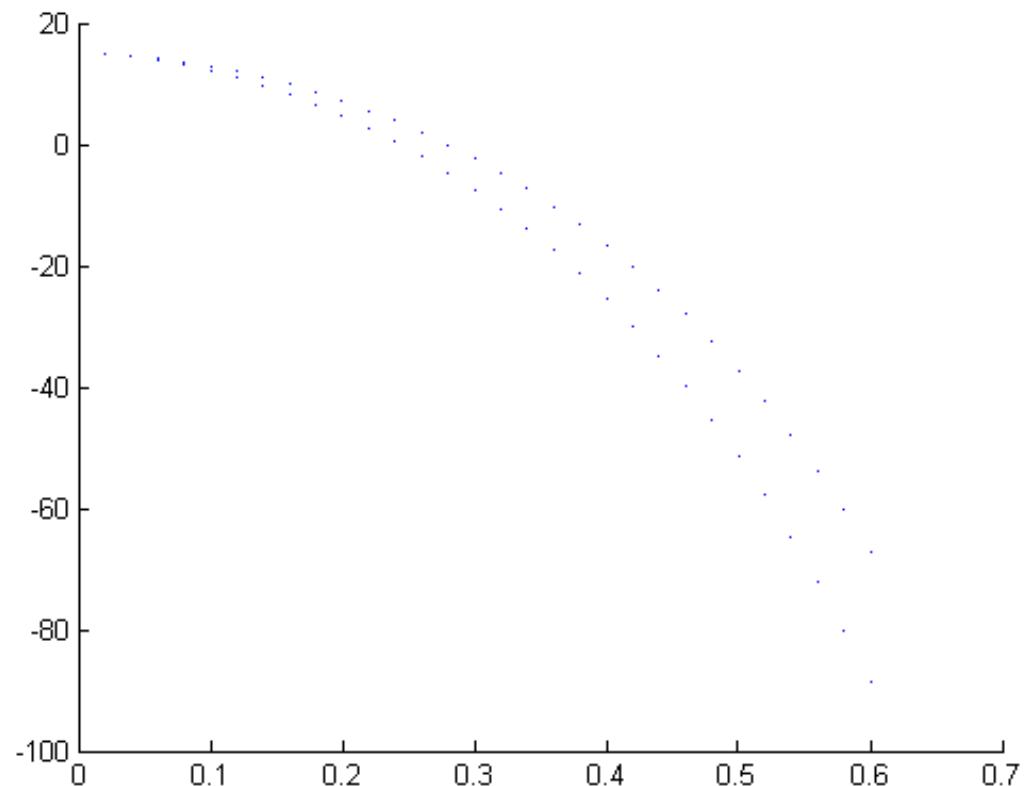
P1c=14.7+(nPressure-14.7);
P1x=14.7-(nPressure-14.7);

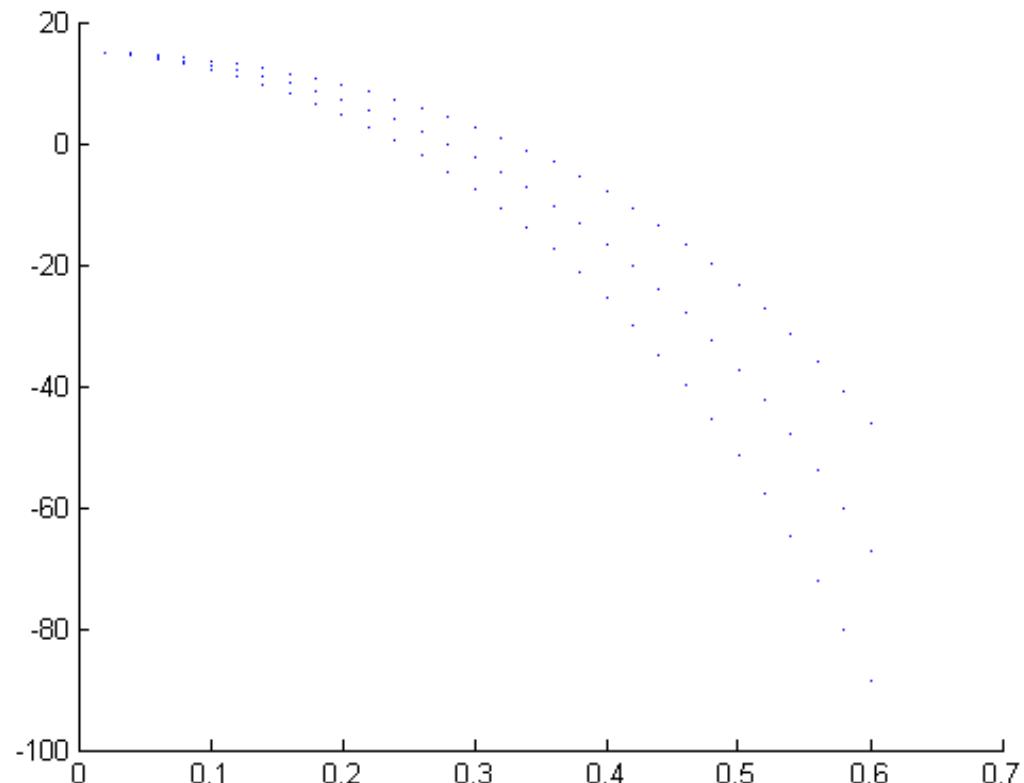
% plot the point
hold on
plot(z,nPressure, '-')

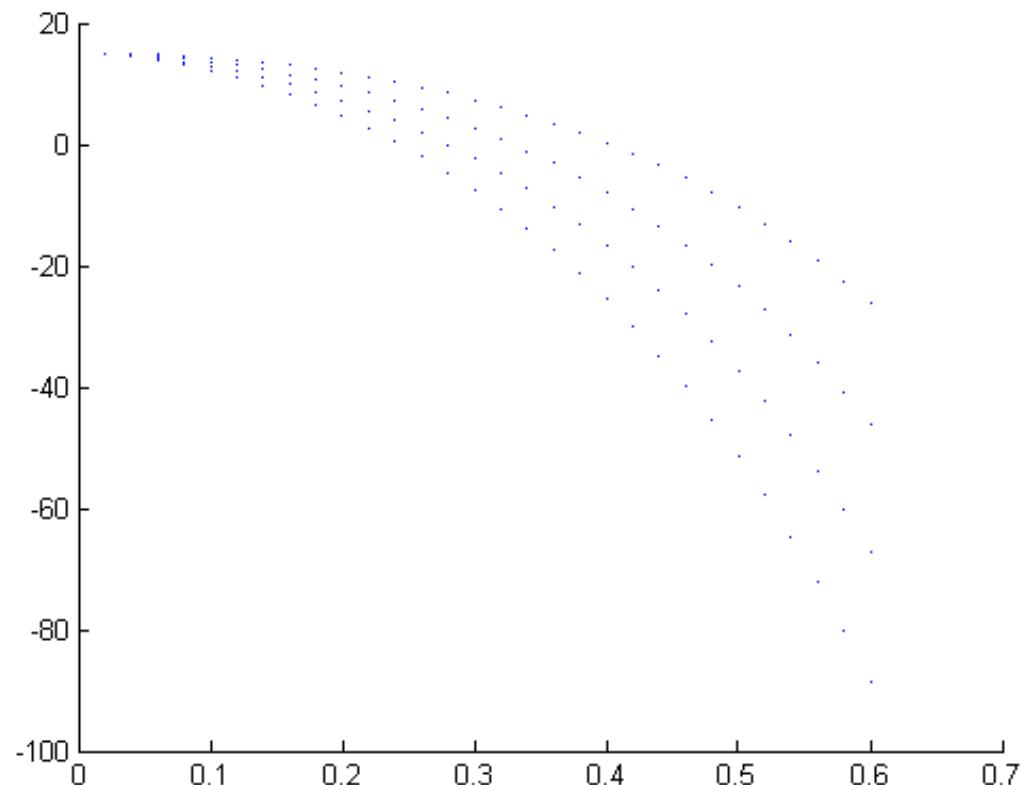
end

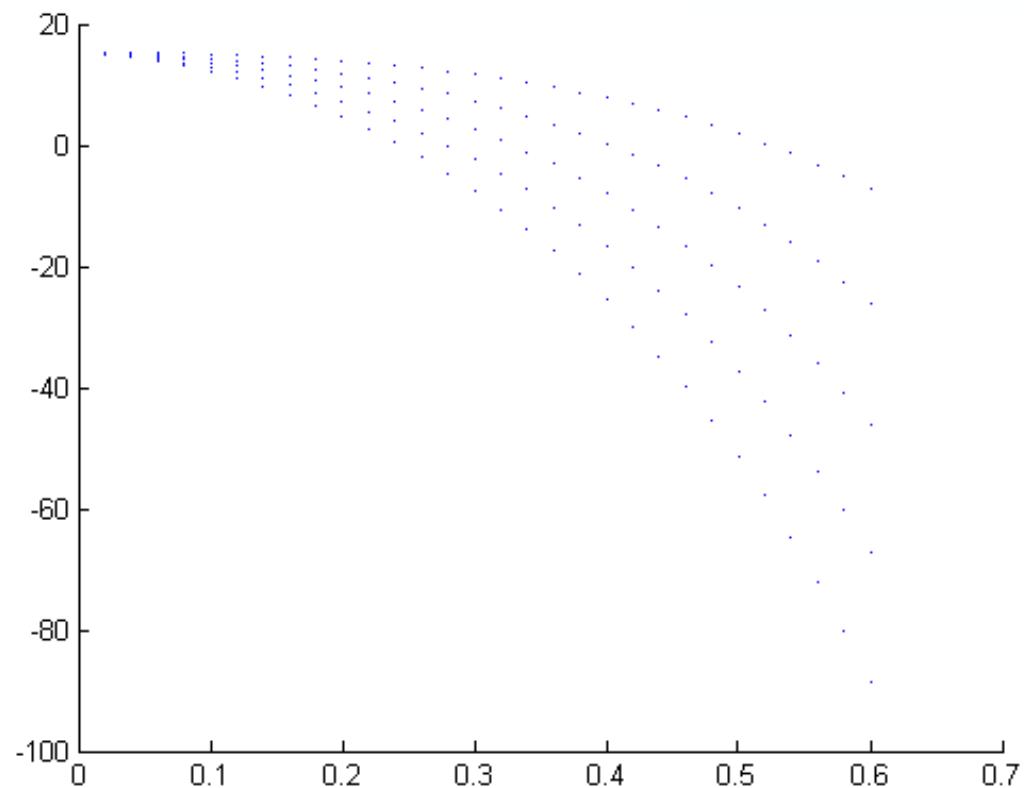
% go back and redo process for next diameter
```

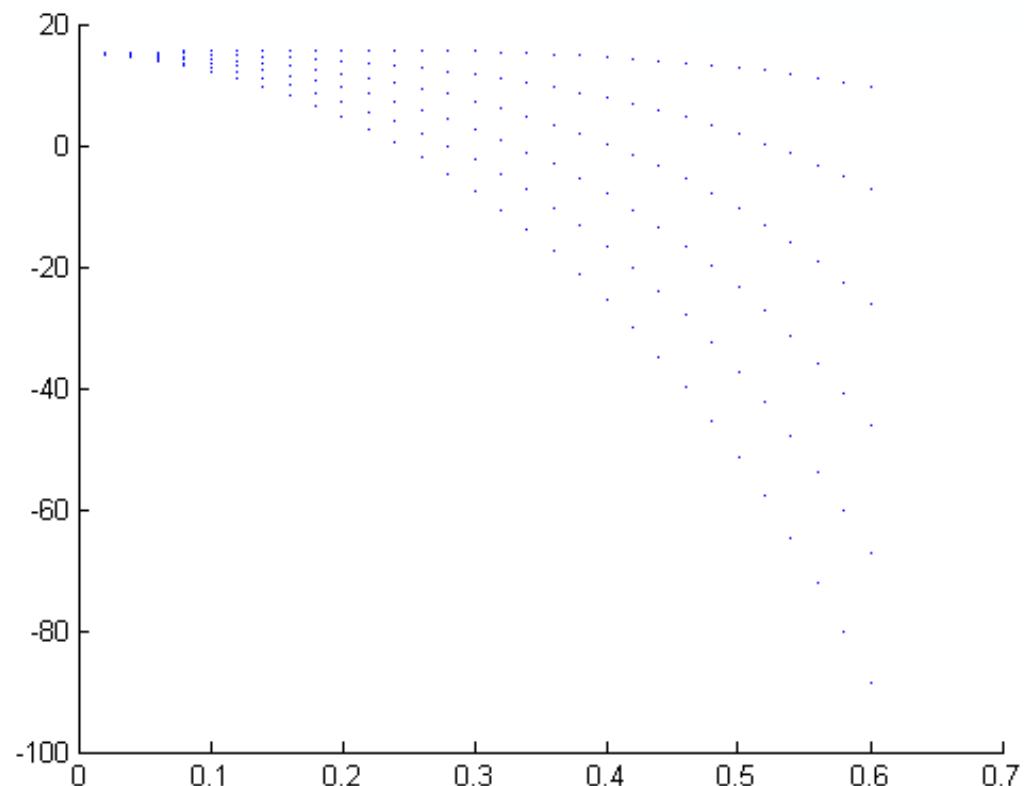


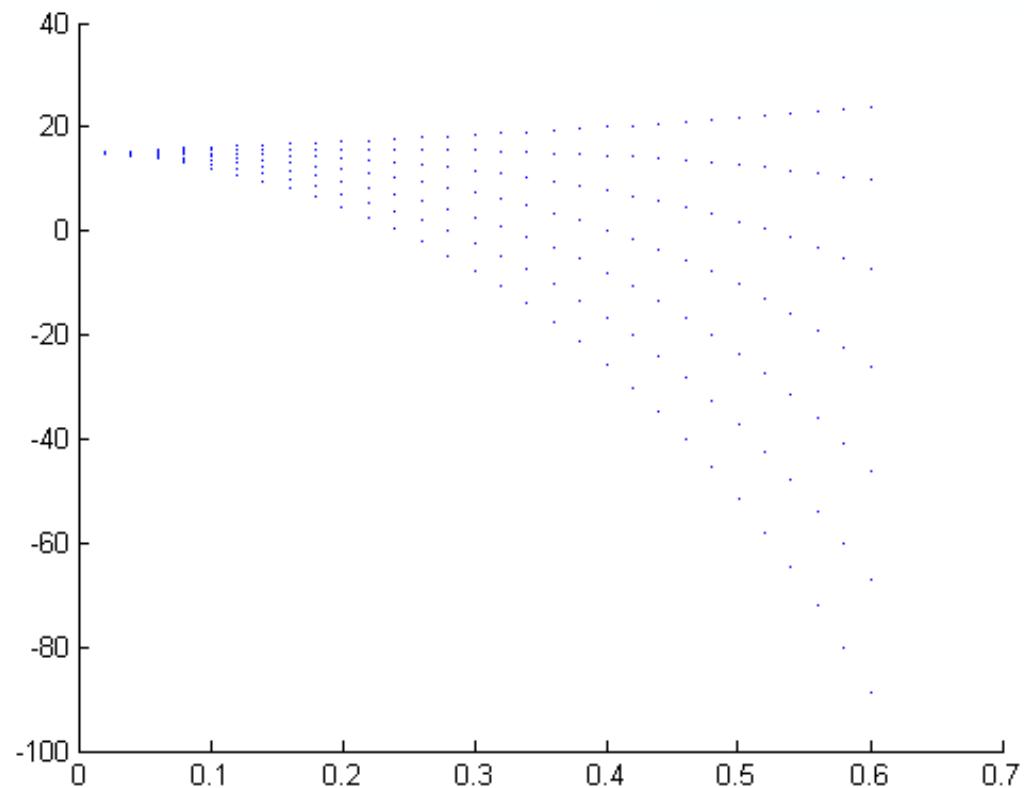


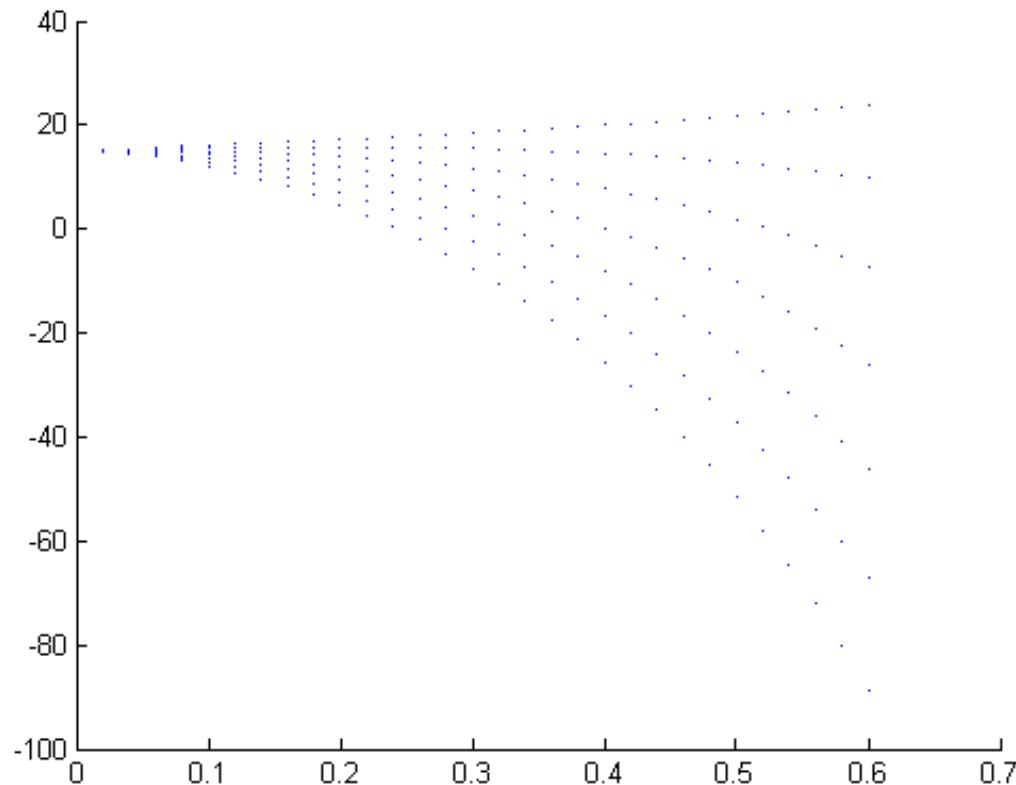












```
end

% plot everthing
plot([0, .6], [14.97, 14.97], '-');
axis([0,.6,-14,40])
hold off
```

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