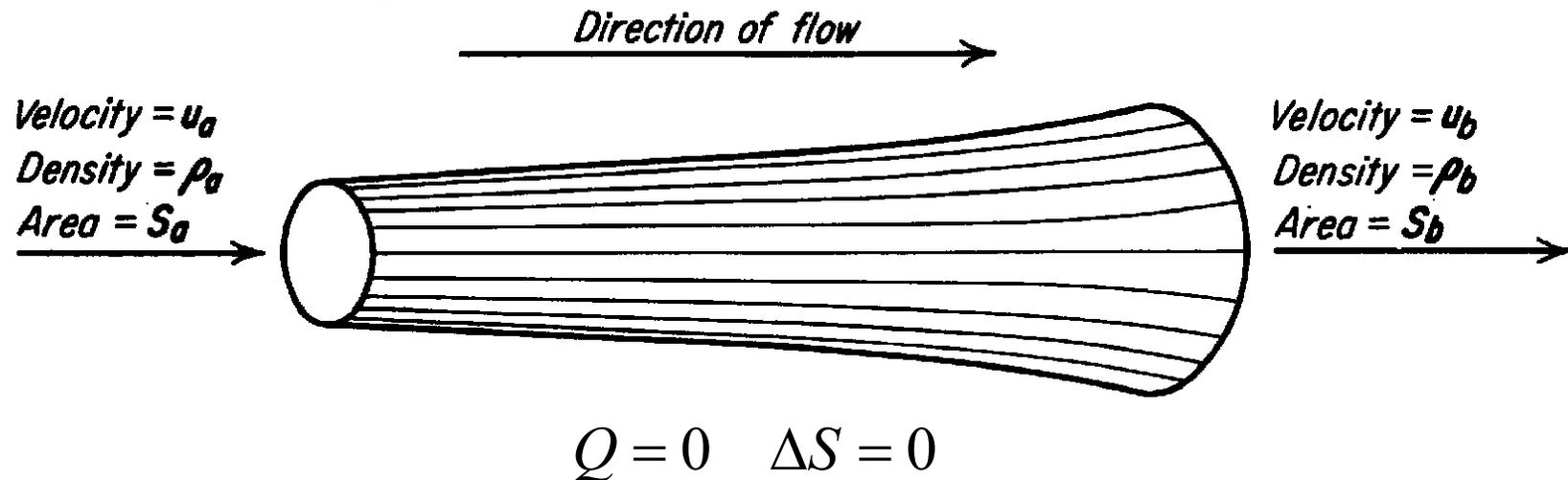


Isentropic Flow of Inviscid Fluid



In this case The mass balance and MEB are the same as that for the isothermal case.

Now though the total energy balance will give a relation between the velocity and temperature

Equation of State

$$\frac{1}{p} \frac{dp}{dx} - \frac{1}{\rho} \frac{d\rho}{dx} - \frac{1}{T} \frac{dT}{dx} = 0$$

Given the normal equation of state, the TEB, MEB, and the thermodynamic relation $C_p - C_v = zR/M$, isentropic flow gives the following useful values.

Useful Relationships

Given the normal equation of state, the TEB, MEB, and the thermodynamic relation $C_p - C_v = zR/M$, isentropic flow gives the following useful values.

$$pV^\gamma = p_0V_0^\gamma$$

$$\frac{p}{\rho^\gamma} = \frac{p_0}{\rho_0^\gamma}$$

$$\gamma = \frac{C_p}{C_v}$$

$$\frac{p}{p_0} = \left(\frac{T}{T_0} \right)^{\gamma/(\gamma-1)}$$

From Mechanical Energy Balance

$$u \frac{du}{dx} + \frac{1}{\rho} \frac{dp}{dx} = 0 \quad \text{or} \quad u du + \frac{1}{\rho} dp = 0$$

$$u du = -\frac{1}{\rho} dp = -\left[\rho_0 \left(\frac{p}{p_0} \right)^{1/\gamma} \right]^{-1} dp$$

Integrating

$$u^2 - u_0^2 = \frac{2p_0\gamma}{\rho_0(\gamma-1)} \left[1 - \left(\frac{p}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right] \quad \leftarrow u \leftrightarrow p$$

Isentropic Flow

$$u^2 - u_0^2 = \frac{2zRT_0}{M} \frac{\gamma}{(\gamma - 1)} \left[1 - \left(\frac{T}{T_0} \right) \right] \quad \leftarrow u \leftrightarrow T$$

$$u^2 - u_0^2 = \frac{2p_0\gamma}{\rho_0(\gamma - 1)} \left[1 - \left(\frac{\rho}{\rho_0} \right)^{\gamma-1} \right] \quad \leftarrow u \leftrightarrow \rho$$

Velocity, N_{Ma} , and Stagnation

For isentropic flow the definition of the speed of sound is:

$$u_{s,s} \equiv \sqrt{\left(\frac{dp}{d\rho}\right)_s} = \sqrt{\frac{\gamma p}{\rho}} = \sqrt{\frac{\gamma RT}{M}}$$

It is also convenient to express the relationships in terms of a reference state where $u_0 = 0$. This is called the stagnation condition ($u_0 = 0$) and P_0 and T_0 are the stagnation pressure and temperature.

Velocity – Mach Relationships

The previous relationships now become:

$$N_{Ma}^2 = \frac{2}{\gamma - 1} \left[\left(\frac{p_0}{p} \right)^{\frac{\gamma - 1}{\gamma}} - 1 \right]$$

and

$$N_{Ma}^2 = \frac{2}{\gamma - 1} \left[\left(\frac{T_0}{T} \right) - 1 \right]$$



Cross-Sectional Area for Sonic Flow

Application of the continuity (mass balance) equation gives:

$$\frac{S}{S^*} = \frac{1}{N_{Ma}} \left[\frac{2 + (\gamma - 1)N_{Ma}^2}{\gamma + 1} \right]^{(\gamma + 1)/2(\gamma - 1)}$$

S^* is a useful quantity. It is the cross-sectional area that would give sonic velocity ($N_{Ma} = 1$).

Summary of Equations for Isentropic Flow

$$\frac{S}{S^*} = \frac{1}{N_{Ma}} \left[\frac{2 + (\gamma - 1)N_{Ma}^2}{\gamma + 1} \right]^{(\gamma+1)/2(\gamma-1)} \quad \frac{p}{p_0} = \left[1 + \frac{(\gamma - 1)}{2} N_{Ma}^2 \right]^{\gamma/(1-\gamma)}$$

$$\frac{T}{T_0} = \left[1 + \frac{(\gamma - 1)}{2} N_{Ma}^2 \right]^{-1} \quad \frac{\rho}{\rho_0} = \left[1 + \frac{(\gamma - 1)}{2} N_{Ma}^2 \right]^{1/(1-\gamma)}$$

p_0 , T_0 , ρ_0 , are at the stagnant (reservoir) conditions.

These ratios are often tabulated versus N_{Ma} for air ($\gamma = 1.4$).
One must use the equations for gases with $\gamma \neq 1.4$.

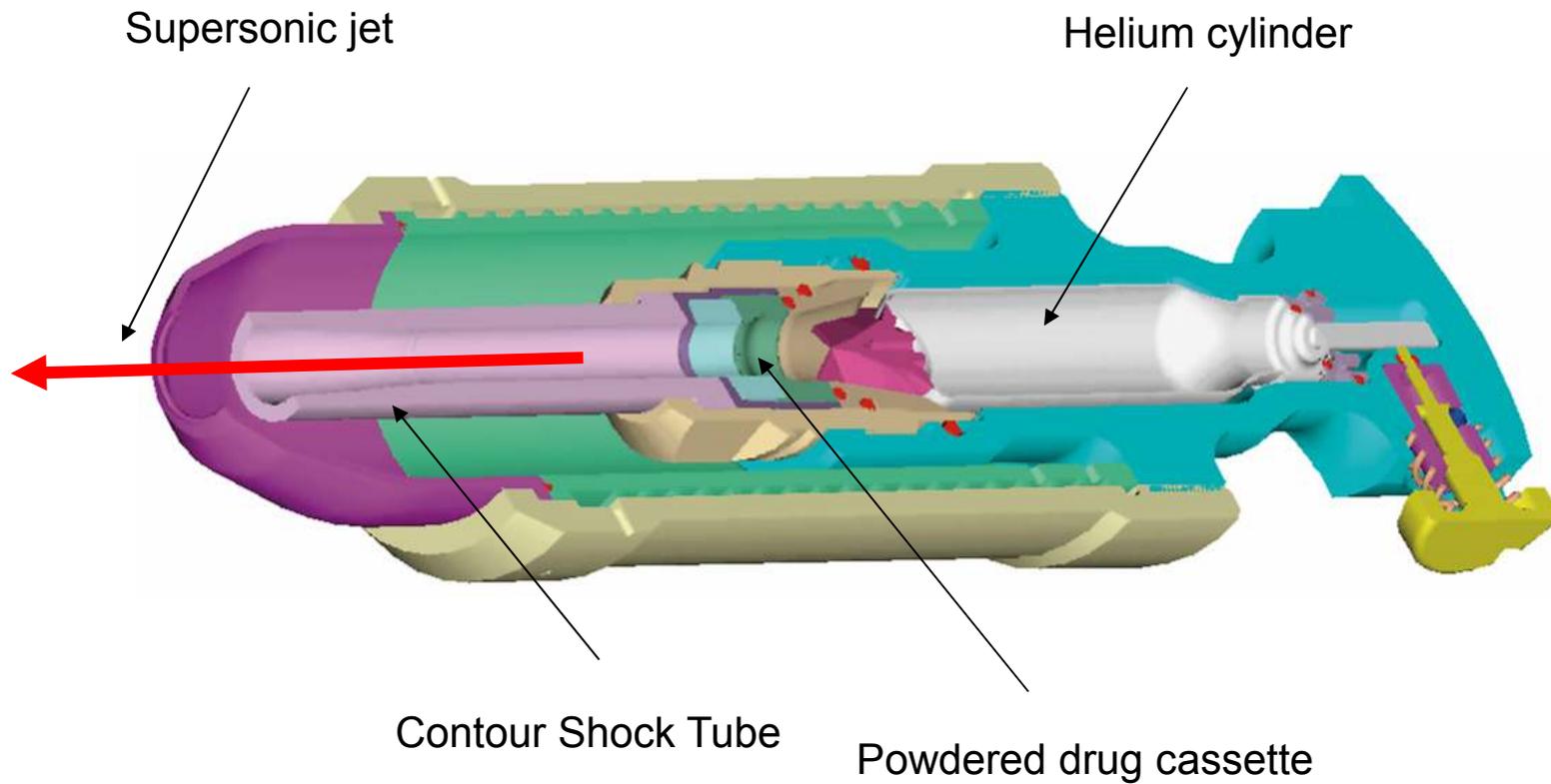
Maximum Mass Flow Rate

Since the maximum velocity at the throat is $N_{Ma} = 1$, there is a maximum flow rate:

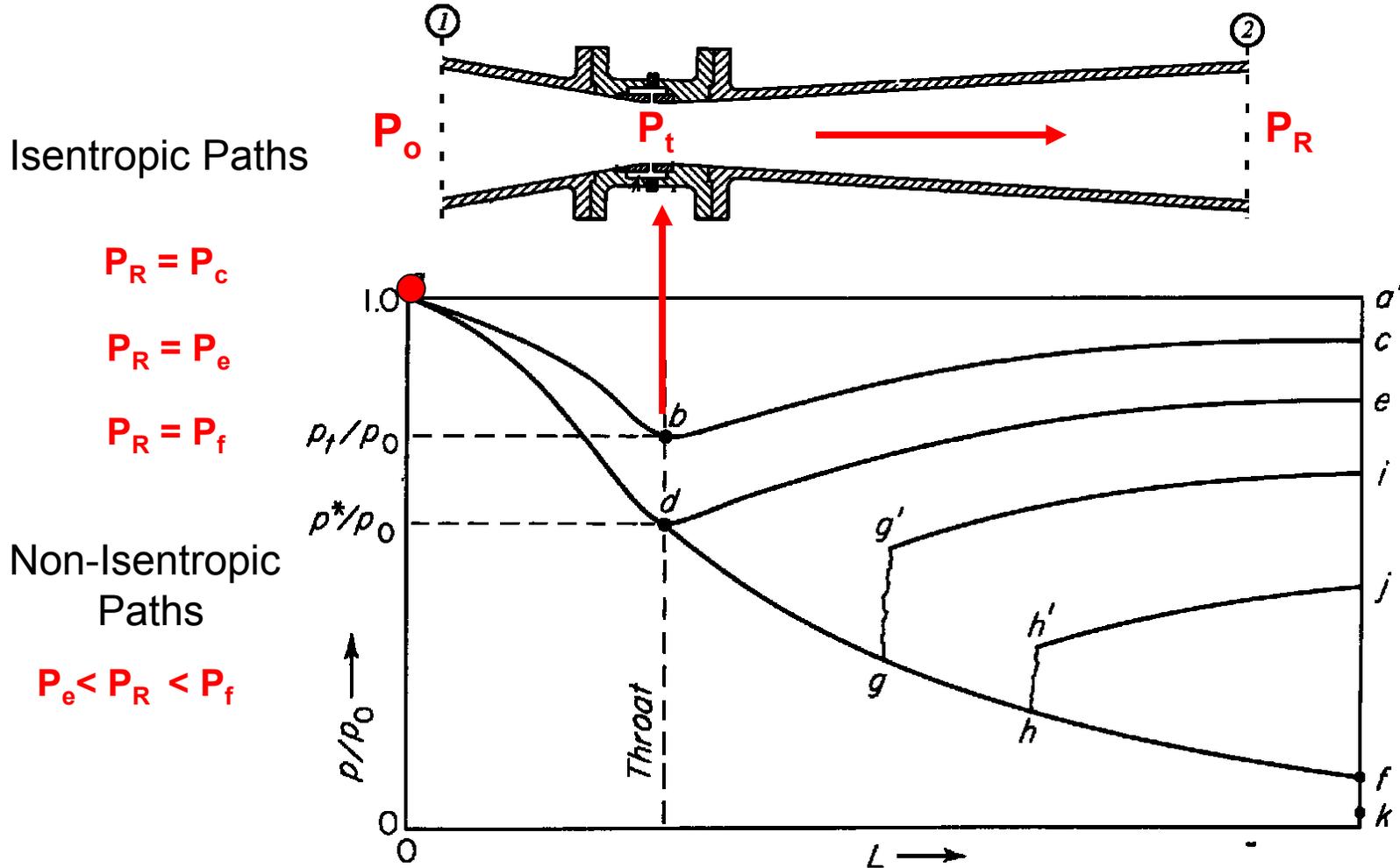
$$\dot{m}_{\max} = S^* \sqrt{\gamma \rho_0 p_0 \left[\frac{2}{\gamma + 1} \right]^{\frac{(\gamma+1)}{(\gamma-1)}}}$$

Increase flow by making throat larger, increasing stagnation pressure, or decrease stagnation temperature. Receiver conditions do not affect mass flow rate.

Drug Injection via Converging / Diverging Nozzle



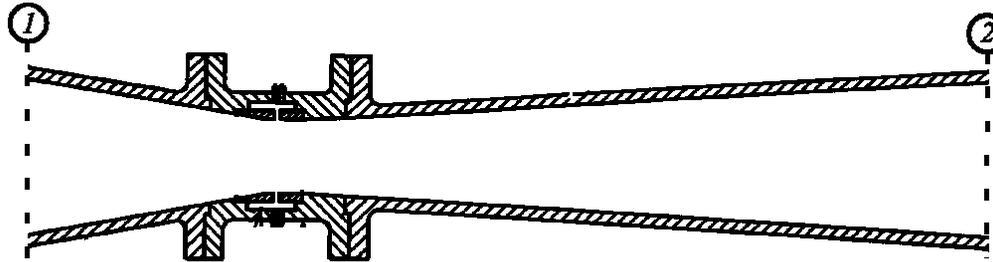
Shock Behavior



Sonic Flow at throat (maximum mass flowrate)



10 Minute Problem



Air flows from a large supply tank at 300 F and 20 atm (absolute) through a converging-diverging nozzle. The cross-sectional area of the throat is 1 ft² and the velocity at the throat is sonic. A normal shock occurs at a point in the diverging section of the nozzle where the cross-sectional area is 1.18 ft². The Mach number just after the shock is 0.70.

What would be the pressure (P_1) at $S = 1.18 \text{ ft}^2$ if no shock occurred ?

What are the new conditions (T_2 and P_2) after the shock ?

What is the Mach number and pressure at a point in the diverging section of the nozzle where the cross-sectional area is 1.8 ft² ?